

ABSTRACT

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## ABSTRACT

Solid fuel rocket engines are one of the most reliable and efficient propulsion systems used to lift payloads into orbit, in terms of  $\lambda = (\square + \diamond)\psi$ . Used throughout the astrodynamics community, the theory of the flow within the motor chamber is in fact a black art which defies all attempts at analysis.

The present work (no exception to the statement above) contains a theoretical and numerical approach to the flow of the gases within the motor chamber. The shape of the chamber and original fuel configuration, and the patterns of combustion and flow/expulsion of gases, are modelled by a system of thirty fourth-degree differential equations.

$$f_i^{(34)}(x, y, z, t) = \sum_{j=0}^{33} a_{ij} f_i^{(j)}(x, y, z, t)$$

Acceptable numerical solutions would require one thousand pentium processors working day and night for  $10^{11.2}$  years.

NORTHERN ILLINOIS UNIVERSITY

FIVE-DIMENSIONAL FLOW IN SOLID FUEL ROCKET ENGINES

A DISSERTATION SUBMITTED TO THE GRADUATE SCHOOL  
IN PARTIAL FULFILLMENT OF THE REQUIREMENTS  
FOR THE DEGREE  
DOCTOR OF PHILOSOPHY

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BY

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Certification:

In accordance with departmental and Graduate  
School policies, this dissertation is accepted in  
partial fulfillment of degree requirements

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Dissertation Director

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Date

## **DEDICATION**

To all of the fluffy kitties.

## **ACKNOWLEDGEMENTS**

Here's where you acknowledge folks who helped.

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# CHAPTER 1

## INTRODUCTION

This sample document illustrates how to use the `niuthesis` class. Some requirements of the Graduate School are written into that file; page size, line spacing, appropriate placement of captions for tables and figures, etc. Other tasks of conforming to the requirements are left to other existing L<sup>A</sup>T<sub>E</sub>X packages.

### 1.0.1 Question: What are the issues in studying this subject?

A major goal in studying solid fuel rocket motors is to create a model of the dynamics of a motor chamber. This involves two major goals: the combustion zone and the acoustic zone. Figure ?? shows this. The combustion zone consists of the thin layer above the solid fuel where the gasification of the fuel takes places. The zone is very reactive and highly turbulent. The acoustic-vortical zone is the volume of gas above the combustion zone. Within this zone, the gas is non-reactive and contains acoustic waves and vorticity.

The work presented here<sup>1</sup> is an extension of Lao[6] and Lao et al.[7] The driving frequency is on the order of the inverse of the axial acoustic time scale,  $t'_A = L'/C'_0$ , where  $L'$  is the length of the cylinder and  $C'_0$  is the reference speed of sound.<sup>2</sup> Radial and azimuthal velocities<sup>5</sup> are found to vanish exponentially fast in the downstream direction, as suggested by Table 1.0.1.

---

<sup>1</sup>Footnotes are handled neatly by L<sup>A</sup>T<sub>E</sub>X.

<sup>2</sup>Remember the traditional method of calculating the distance of lightning? See the flash, count seconds until you hear the thunder, divide by five, that's the number of miles. That assumes  $C_0 = \frac{1mi.}{5s}$ .

<sup>5</sup>gratuitous footnote

Table 1.1: Here is an example of a table with its own footnotes. Don't use the `\footnote` macro if you don't want the footnotes at the bottom of the page. Also, note that in a thesis the caption goes *above* a table, unlike figures.

wave form	$S$ (kVA)	$P$ (kW)	$Q^*$ (kVAr)	$D^\dagger$ (kVAd)
	25.87	25.83	1.3	$\approx 0$
	25.48	25.00	-2.82	4.03
	25.11	18.02	-9.75	14.52
Table 2	24.98	22.26	9.19	6.64
Fig. ??	23.48	15.00	6.59	16.82
Fig. 2.1	24.64	22.81	-0.44	9.3
Fig. ??	23.03	18.01	3.36	13.95

\*kVAr means reactive power.

†kVAd means distortion power.

These results provide an analytical explanation of those found from computational analysis by Fabnis et al.[4] The non-axisymmetric flow near the endwall contains cross-sectional velocity patterns that include flow across the cylinder axis. A viscous boundary layer adjacent to the sidewall and near the endwall is studied to find the transition between the transient core flow and the no-slip condition on the sidewall. It is found, as in Lao et al.[7], that the azimuthal component of the vorticity is proportional to the inverse of the Mach number. In addition, the axial component of the vorticity driven by the non-axisymmetric boundary condition at the endwall is also found to be proportional to the the inverse of the Mach number.

## CHAPTER 2

### MATHEMATICAL FORMULATION

The objective of this fake thesis document is to demonstrate a some L<sup>A</sup>T<sub>E</sub>X features as well as features specific to the thesis class. We start by giving one short formula,

$$A = \pi r^2 \tag{2.1}$$

and one big hairy multi-line formula (one of the non-dimensional Navier-Stokes equations):

$$\begin{aligned} \rho \left[ \frac{DV_r}{Dt} - M\epsilon^2 \frac{V_\theta^2}{r} \right] = & -\frac{\delta^2}{\gamma M} \frac{\partial P}{\partial r} + \frac{M \delta^2}{Re} \left\{ 2 \frac{\partial}{\partial r} \left[ \mu \left( \frac{\partial V_r}{\partial r} - \frac{1}{3} \nabla \cdot \bar{\mathbf{V}} \right) \right] \right. \\ & + \frac{1}{r} \frac{\partial}{\partial \theta} \left[ \mu \left( \frac{1}{r} \frac{\partial V_r}{\partial \theta} + \epsilon \frac{\partial V_\theta}{\partial r} - \epsilon \frac{V_\theta}{r} \right) \right] \\ & + \frac{\partial}{\partial z} \left[ \mu \left( \frac{1}{\delta^2} \frac{\partial V_r}{\partial z} + \frac{\partial V_z}{\partial r} \right) \right] \\ & \left. + 2 \frac{\mu}{r} \left[ \frac{\partial V_r}{\partial r} - \frac{\epsilon}{r} \frac{\partial V_\theta}{\partial \theta} - \frac{V_r}{r} \right] \right\}, \end{aligned} \tag{2.2}$$

The latter equation is non-dimensionalized using the following definitions:

$$r = \frac{r'}{R'}, \quad z = \frac{z'}{L'}, \quad t = \frac{t'}{t'_a}, \quad \kappa = \frac{\kappa'}{\kappa'_0}, \quad \mu = \frac{\mu'}{\mu'_0}, \quad C_V = \frac{C'_V}{C'_{V0}},$$

where  $P'_0$  is the initial static pressure in the cylinder, and  $\rho'_0$  and  $T'_0$  are the density and temperature of the fluid being injected from the sidewall. The aspect ratio is given by  $\delta = \frac{L'}{R'}$ , where  $\delta \gg 1$ . The induced characteristic axial velocity and the characteristic endwall velocity disturbance  $V'_{z0}$  is defined with respect to the injection reference sidewall velocity,  $V'_{r0}$  by overall mass conservation,  $\frac{V'_{z0}}{V'_{r0}} = \delta$ . The size of the initially unknown

Table 2.1: This is a table constructed with `\LaTeX` commands in the `tabular` environment.

n	$n^2$	$n^3$	$n^4$	$n^7$	$n^{13}$
2	4	8	16	128	8192
3	9	27	81	2187	1594323
4	16	64	256	16384	67108864
5	25	125	625	78125	1220703125
6	36	216	1296	279936	13060694016
7	49	343	2401	823543	96889010407

reference azimuthal velocity  $V'_{\theta 0}$  is related to  $V'_{r0}$  by  $\frac{V'_{\theta 0}}{V'_{r0}} = \epsilon$ . Later, it is shown that  $\epsilon = 1$ .

The time is non-dimensionalized using the axial acoustic time scale,  $t'_a = \frac{L'}{C'_0}$ , where  $C'_0 = (\gamma \mathcal{R}' T'_0)^{\frac{1}{2}}$  is the speed of sound<sup>1</sup>,  $\mathcal{R}'$  is the gas constant, and  $\gamma$  is the ratio of specific heats. Also the Reynolds number, Wrenchl number, and Mock number are defined as

$$Re = \frac{\rho' V'_{z0} L'}{\mu'_0}, \quad Wr = \frac{\mu'_0 C'_{p0}}{\kappa'_0}, \quad M = \begin{pmatrix} V'_{z0} \\ C'_0 \end{pmatrix} \cdot \begin{pmatrix} 8a & z_0 - \rho \\ 2 & z_0 - \mu \end{pmatrix} \begin{pmatrix} Wr \\ p - 7 \end{pmatrix}$$

where  $Re \ll 1$ ,  $M \gg 1$ , and  $Wr = O(1)$ .

Here is an example of using the macros `\singlespacing` and `\doublespacing`:

This paragraph was preceded by the command `\singlespacing`. The Mock number is chosen as a small parameter to model the small magnitude found in a typical rocket motor chamber, as opposed to the rocket nozzle where larger values are possible<sup>2</sup>. The aspect ratio,  $\delta$ , is taken to be a large parameter, because many chambers have aspect ratios between 15 and 50. Now the command “`\doublespacing`”:

The following table is created using the `\LaTeX` `tabular` environment.

However, sometimes you want to use a table produced by some other software, such as Excel. If the table is saved to a PostScript file, then it can be displayed using the

`\includegraphics` macro inside a `table` environment:

---

<sup>1</sup>In air at 1 atm.,  $\frac{1mi.}{5s}$ .

<sup>2</sup>Not just possible, desirable!

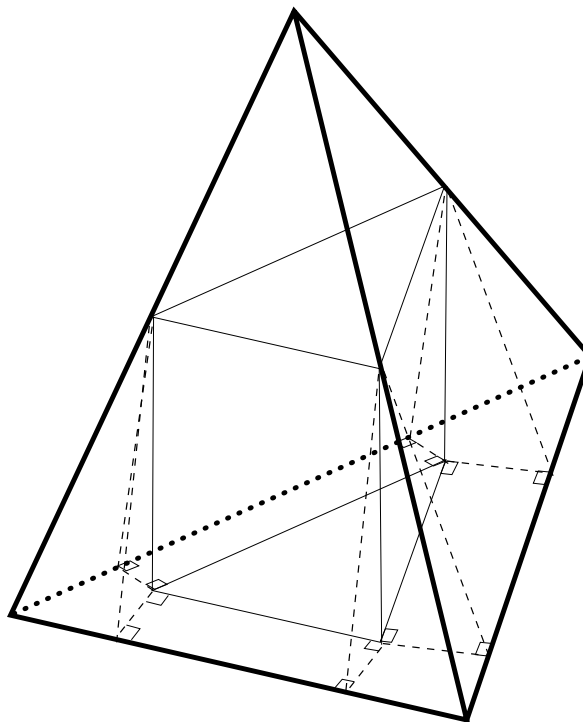


Figure 2.1: A triangular pyramid may be cut up as shown, to yield one top pyramid (with one-eighth the volume of the full pyramid), three bottom corner pyramids (which, when joined, are congruent to the top pyramid), three prisms along the bottom edges (the area of whose bottom faces total  $B/2$ ) and the large central prism (volume =  $(B/4)(h/2) = Bh/8$ ). The image, from PostScript file “pyr.ps”, was read in using the `\includegraphics` command, from the `graphicx` package.

Table 2.2: This table wasn’t constructed with  $\text{\LaTeX}$  commands, but resides in a PostScript file (`tableD.ps`) created by some other software.

<b>n</b>	<b>n<sup>2</sup></b>	<b>n<sup>3</sup></b>	<b>n<sup>4</sup></b>	<b>n<sup>7</sup></b>	<b>n<sup>13</sup></b>
2	4	8	16	128	8192
3	9	27	81	2187	1594323
4	16	64	256	16384	67108864
5	25	125	625	78125	1220703125
6	36	216	1296	279936	13060694016
7	49	343	2401	823543	96889010407

## 2.1 Conditions for Catastrophic Combustion

Initially, a steady flow is generated by the sidewall injection,  $V_r = -V_{rws}(z)$ . The subscript *srw* is used to mean that there is a steady radial wall velocity. The sign is negative due to the injection toward centerline. At  $t = 0^+$ , the endwall begins oscillating with the non-dimensionalized sinusoidal axial velocity,  $V_z = \tilde{F}_{rw}(r, \theta, t)$ , for  $\omega = O(1)$ . Figure ?? conforms to these thesis specs: “Figures are placed immediately after their first mentions . . . Figure captions appear below figures and are typed in the same style and size as the text. Captions should fit within the standard margins and are not reduced if the figures are reduced . . . Figures may be printed broadside, with the top toward the left margin; the caption then appears beneath the figure and is typed from bottom to top of the page within the standard margins. . . .”

Some of the boundary conditions are:

$$z = 0; \quad V_z = \begin{cases} 0, & t \leq 0 \\ \tilde{F}_{zw}(r, \theta, t), & t > 0 \end{cases} \quad (2.3)$$

$$z = 0; \quad V_\theta = V_r = 0 \quad (2.4)$$

$$r = 0; \quad P, \rho, T, V_r, V_\theta, V_z \text{ finite}, \quad (2.5)$$

$$r = 1; \quad V_r = F_{rws}(z), \quad (2.6)$$

$$r = 1; \quad V_z = V_\theta = 0, \quad (2.7)$$

and solutions must be periodic in  $\theta$ .







This is the third paragraph of the subsection. Filler filler filler filler filler filler filler filler. Filler filler filler filler filler filler filler filler.

#### **2.2.3.1 This is a subsection (1)**

This is the first paragraph of the subsection. Whether it is numbered or inlined depends on the option selected at the beginning of the thesis.

By default, a `\subsection` heading is numbered and set off on a separate line, left-justified.

**However.** Using the `inlineh4` option, subsection headers are inlined. And using the `nonumh4` option suppresses numbering of the subsections. Together they make subsection headings just the same as paragraph headings.

#### **2.2.3.2 This is another subsection (2)**

Once again, whether its heading is numbered and/or inlined depends on the class options chosen at the start.

There is no “subsubsection” entity, and “subparagraph” gets no special treatment in *thesis* class.

### **2.3 The End**

Finally, this is the end. The bibliography starts on the next page.

## REFERENCES

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**APPENDIX A**  
**OBJECTIVE SYMPTOMS**

Appendices follow the same page-numbering rules as regular chapters. The first page of a multi-page appendix is not numbered. But the page of a single-page appendix *is* numbered.

**Are they slow learners** or is it a *REAL* problem? These are classic findings in the hopelessly computer challenged.

1. Can't copy from hard drive to disk.
2. Can't eject disks.
3. The word "disk" has thousands of meanings to them. None are correct.
4. Saving a document in any form is a concept totally unexplainable to them.
5. Desktop covered with Untitled Folders - look again, untitled folders are everywhere.
6. "Lost" documents found often in the Apple Menu.
7. Trash always full. Claim they don't know how to place things in trash.
8. Mysterious things happen to their documents or computer when they are not present.  
AKA "computer victims".
9. Highlighting = deleting. Dragging = Oblivion.
10. Selecting, double-clicking a problem? They will always say their mouse is broken.
11. Their double- click mechanics wants you to send them to a neurologist.
12. Computer always on due to fear of having to restart it.
13. Have never read their QuickMail - will say "I prefer a phone call".
14. Have magical beliefs about what computers do.
15. Describes some flaky way computers could REALLY help them, but is not yet available.

16. Constantly saying they need more “memory”.
17. Requests gizmos and gadgets, i.e., “mouse leash” or “disk cozy”.
18. Avoids eye contact when talking about computers.

**APPENDIX B**  
**ODE TO SPOT**

**(Data, Stardate 1403827)** Throughout the ages, from Keats to Giorchamo, poets have composed “odes” to individuals who have had a profound effect upon their lives. In keeping with that tradition I have written my next poem ...in honor of my cat. I call it...Ode...to Spot. (Shot of Geordi and Worf in audience, looking mystified at each other.)

Felus cattus, is your taxonomic nomenclature  
 an endothermic quadruped, carnivorous by nature?  
 Your visual, olfactory, and auditory senses  
 contribute to your hunting skills, and natural defenses.  
 I find myself intrigued by your sub-vocal oscillations,  
 a singular development of cat communications  
 that obviates your basic hedonistic predilection  
 for a rhythmic stroking of your fur to demonstrate affection.  
 A tail is quite essential for your acrobatic talents;  
 you would not be so agile if you lacked its counterbalance.  
 And when not being utilized to aid in locomotion,  
 It often serves to illustrate the state of your emotion.

(Commander Riker begins to applaud, until a glance from Counselor Troi brings him to a halt.) Commander Riker, you have anticipated my denouement. However, the sentiment is appreciated. I will continue.

O Spot, the complex levels of behavior you display  
 connote a fairly well-developed cognitive array.  
 And though you are not sentient, Spot, and do not comprehend  
 I nonetheless consider you a true and valued friend.